

# WAVES IN MATERIALS WITH MICROSTRUCTURE: NUMERICAL SIMULATION

### M.Berezovski, A.Berezovski, J.Engelbrecht

Centre for Nonlinear Studies, Institute of Cybernetics Tallinn University of Technology, Tallinn, Estonia

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M.Berezovski, A.Berezovski, J.Engelbrecht

## Outline



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

Numerical simulations

### Motivation

- Microstructure model
  - Dual internal variables approach
  - Balance laws
- Numerical results
- Conclusion



#### ♦ Outline

#### Motivation

Microstructure

Microstructure

Microstructure

Example of microstructure

behavior

Microstructure model

Dual internal variables approach

Numerical simulations

### **Motivation**

### *Microstructure*



#### ♦ Outline

#### Motivation

- Microstructure
- Microstructure
- Microstructure
   Example of microstructure behavior
- Microstructure model
- Dual internal variables approach
- Numerical simulations



Thin-section photomicrograph of a concrete.

### **Microstructure**



#### ♦ Outline

Motivation

Microstructure

Microstructure

 Microstructure
 Example of microstructure behavior

Microstructure model

Dual internal variables approach

Numerical simulations



The microstructure of the roller ball, which is made of cast iron. The flakes of graphite are surrounded by ferrite, the brown is the pearlite

### *Microstructure*



#### ♦ Outline

**Motivation** 

Microstructure

Microstructure

Microstructure

 Example of microstructure behavior

Microstructure model

Dual internal variables approach

Numerical simulations



Shape memory allow Cu-Al-Ni.

### **Example of microstructure behavior**





Response of two different media on a step-wise loading.



#### ♦ Outline

Motivation

Microstructure model

Wave equation

 Generalized wave equations

Dual internal variables approach

Numerical simulations

### **Microstructure model**

## Wave equation



#### Outline

Motivation

Microstructure model

✤ Wave equation

 Generalized wave equations

Dual internal variables approach

Numerical simulations

### • One-dimensional wave equation

$$u_{tt} = c^2(x)u_{xx}$$

*u* is the displacement, *c* is the elastic wave speed, which is constant for homogeneous medium, but changing at alternating layers in periodic medium.

## **Generalized wave equations**



#### ♦ Outline

Motivation

Microstructure model

Wave equation

 Generalized wave equations

Dual internal variables approach

Numerical simulations

 Linear version of the Boussinesq equation for elastic crystals (cf. Maugin, 1995)

$$u_{tt} = c^2 u_{xx} + c^2 l^2 A_{22} u_{xxxx}$$

where l is an internal length parameter and  $A_{22}$  is dimensionless coefficient

The Love-Rayleigh equation for rods accounting for lateral inertia (cf. Love, 1944)

$$u_{tt} = c^2 u_{xx} + l^2 A_{21} u_{xxtt}$$

This equation is derived also by Maugin (1999); Wang and Sun (2002); Fish et al (2002)

## **Generalized wave equations**



#### Outline

Motivation

Microstructure model

♦ Wave equation

 Generalized wave equations

Dual internal variables approach

Numerical simulations

The more general model combining the two dispersion models (Engelbrecht and Pastrone, 2003)

$$u_{tt} = (c^2 - c_A^2) \ u_{xx} + l^2 A_2 \left( u_{tt} - c^2 A_1 \ u_{xx} \right)_{xx}$$

The Maxwell-Rayleigh model of anomalous dispersion (cf. Maugin, 1995)

$$u_{tt} = c^2 \ u_{xx} + \frac{l^2 A_0}{c^2} \left( u_{tt} - c^2 \ u_{xx} \right)_{tt}$$

## **Generalized wave equations**



#### ♦ Outline

#### Motivation

Microstructure model

Wave equation

 Generalized wave equations

Dual internal variables approach

Numerical simulations

The "causal" model for the dispersive wave propagation (Metrikine, 2006)

$$u_{tt} = c^2 u_{xx} + l^2 A_{21} u_{xxtt} + c^2 l^2 A_{22} u_{xxxx} - \frac{l^2}{c^2} A_{23} u_{ttt}$$

 The most general one-dimensional model (Engelbrecht, Berezovski, Pastrone and Braun, 2005)

$$u_{tt} = (c^2 - c_A^2) \ u_{xx} - p^2 (u_{tt} - c^2 u_{xx})_{tt} + p^2 c_1^2 (u_{tt} - c^2 u_{xx})_{xx}$$

where p is dimensionless coefficient



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

Free energy

A nondissipative case

A nondissipative case

Numerical simulations

## **Dual internal variables approach**

### Free energy



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

#### Free energy

A nondissipative case
A nondissipative case

Numerical simulations

 The simplest free energy dependence is a quadratic function (Engelbrecht et al., 2005)

$$\overline{W} = \frac{\rho_0 c^2}{2} u_x^2 + A\alpha u_x + \frac{1}{2} B\alpha^2 + \frac{1}{2} C\alpha_x^2 + \frac{1}{2} D\beta^2$$

where  $\rho_0$  is the matter density, *A*,*B*,*C* and *D* are material parameters,  $\alpha$  and  $\beta$  are internal variables.

### Stress components

 $\sigma = \frac{\partial \overline{W}}{\partial u_x} = \rho_0 c^2 u_x + A\alpha, \quad \eta = -\frac{\partial \overline{W}}{\partial \alpha_x} = -C\alpha_x$ 

## A nondissipative case



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

Free energy

A nondissipative case

A nondissipative case

Numerical simulations

### Interactive internal force

$$\tau = -\frac{\partial \overline{W}}{\partial \alpha} = -Au_x - B\alpha$$

Evolution equations in nondissipative case

$$\alpha_t = -RD\beta, \quad \beta_t = -R(\tau - \eta_x)$$

where *R* is a coefficient

(Van, Berezovski, Engelbrecht, 2008)

Evolution equation for the primary internal variable

$$\alpha_{tt} = R^2 D(\tau - \eta_x)$$

## A nondissipative case



#### ✤ Outline

Motivation

Microstructure model

Dual internal variables approach

Free energy

A nondissipative case

♦ A nondissipative case

Numerical simulations

### • Equations of motion in terms of stresses

$$\rho_0 u_{tt} = \sigma_x$$

$$I\alpha_{tt} = -\eta_x + \tau$$

where  $I = 1/(R^2D)$ .

It is worth to note that the same equations are derives in (Engelbrecht, Cermelli and Pastrone, 1999) based on different considerations.

## A nondissipative case



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

Free energy

A nondissipative case

 A nondissipative case

Numerical simulations

### • Equations of motion

$$\rho_0 u_{tt} = \rho_0 c^2 u_{xx} + A \alpha_x$$

$$I\alpha_{tt} = C\alpha_{xx} - Au_x - B\alpha$$

### • First space derivative of the primary internal variable

$$\alpha_x = -\frac{I}{B}\alpha_{ttx} + \frac{C}{B}\alpha_{xxx} - \frac{A}{B}u_{xx}$$

### • Third derivatives

$$\frac{A}{\rho_0} \alpha_{xxx} = (u_{tt} - c^2 u_{xx})_{xx}, \quad \frac{A}{\rho_0} \alpha_{ttx} = (u_{tt} - c^2 u_{xx})_{tt}$$

## **Generalized wave equation**



#### ♦ Outline

**Motivation** 

Microstructure model

Dual internal variables approach

Free energy

A nondissipative case

 A nondissipative case

Numerical simulations

### • Generalized wave equation

$$u_{tt} = c^2 u_{xx} + \frac{C}{B} \left( u_{tt} - c^2 u_{xx} \right)_{xx} - \frac{I}{B} \left( u_{tt} - c^2 u_{xx} \right)_{tt} - \frac{A^2}{\rho_0 B} u_{xx}$$

 Most general model (Engelbrecht, Berezovski, Pastrone and Braun, 2005)

$$u_{tt} = (c^2 - c_A^2) \ u_{xx} - p^2 (u_{tt} - c^2 u_{xx})_{tt} + p^2 c_1^2 (u_{tt} - c^2 u_{xx})_{xx}$$

### • Identification:

$$A^2 = c_A^2 B \rho_0, \quad C = I c_1^2, \quad B = I / p^2$$



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

Numerical simulations

Conservation laws
 Numerical simulations

 Modification of microstructure model

Cubic nonlinearity

Conclusions

## **Numerical simulations**

## **Equations of motion**



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

Numerical simulations

- Conservation laws
  Numerical
- simulations
- Modification of microstructure model
- Cubic nonlinearity
- Conclusions

### • Equations of motion

$$\rho_0 u_{tt} = \rho_0 c^2 u_{xx} + A \alpha_x$$

$$I\alpha_{tt} = C\alpha_{xx} - Au_x - B\alpha$$

Introducing microvelocity  $\omega$  as follows:

$$\omega_x := -RD\beta$$

### **Conservation laws**



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

Numerical simulations

Conservation laws

Numerical simulations

 Modification of microstructure model

Cubic nonlinearity

Conclusions

### Macromotion

Balance of linear momentum

$$\rho_0 v_t = \rho_0 c^2 \varepsilon_x + A \alpha_x$$

Kinematic compatibility

 $\varepsilon_t = v_x$ 

Microstructure evolution

$$Iw_t = C\alpha_x - \int (A\varepsilon + B\alpha)dx$$

Kinematic compatibility at micro-level

$$\alpha_t = w_x$$

M.Berezovski, A.Berezovski, J.Engelbrecht





M.Berezovski, A.Berezovski, J.Engelbrecht



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

Numerical simulations

Conservation laws

Numerical simulations

 Modification of microstructure model

Cubic nonlinearity

Conclusions

### Scattering of a pulse by a periodic multilayer







M.Berezovski, A.Berezovski, J.Engelbrecht





## Modification of microstructure model



#### Outline

**Motivation** 

Microstructure model

Dual internal variables approach

Numerical simulations

Conservation laws
 Numerical

simulations

 Modification of microstructure model

Cubic nonlinearity

Conclusions

• Changing sign of interactive internal force

$$Iw_t = C\alpha_x + \int (A\varepsilon + B\alpha)dx$$





Waves in materials with microstructure: numerical simulation - 27 / 32





## **Cubic nonlinearity**



#### ♦ Outline

Motivation

Microstructure model

Dual internal variables approach

Numerical simulations

Conservation laws

Numerical

simulations

 Modification of microstructure model

Cubic nonlinearity

Conclusions

### • Free energy function

$$\overline{W} = \overline{W}_{quadratic} + \overline{W}_{cubic}$$

$$\overline{W}_{cubic} = \frac{1}{6}Nu_x^3 + \frac{1}{6}M\alpha_x^3$$

### Equations of motion

$$\rho_0 u_{tt} = \rho_0 c^2 u_{xx} + N u_x u_{xx} + A \alpha_x$$

$$I\alpha_{tt} = C\alpha_{xx} + M\alpha_x\alpha_{xx} + Au_x + B\alpha$$









### **Conclusions**



#### Outline Motivation Microstructure model Dual internal variables approach Numerical simulations Conservation laws Numerical simulations Modification of microstructure model Cubic nonlinearity Conclusions

- Numerical simulations were performed to validate microstructure model
- It is shown that some improvements of model should be made to obtain consistency with direct calculation
  - Further improvements are needed