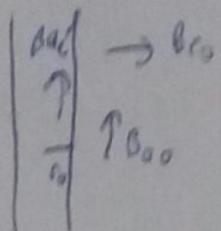


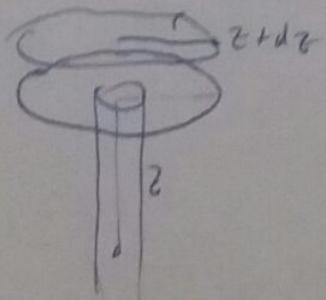
$$\oint H \cdot d\vec{l} = 0 \text{ for this loop } \Rightarrow$$



$$B_{dz} = -H \int_0^\infty \left(\frac{\partial B_{r_0}}{\partial z} \right) dr$$

Since $H \gg 1$ $B_{ac} \gg B_{dd}$

Now if we write $\nabla \cdot \vec{B} = 0$ in an approximate form we get:



$$\phi_{(z)} = \phi_{(z+dz)} + 2\pi r dz B_{r_0}$$

$$-\frac{\partial \phi}{\partial z} = 2\pi r B_{r_0}$$

$$B_{r_0} = -\frac{1}{2\pi r} \frac{\partial \phi}{\partial z} \approx -\frac{1}{2\pi r} \underbrace{\frac{\partial B_{ac}}{\partial z} \pi r_0^2}_{\text{flux inside the cylinder}}$$

$$B_{r_0} \approx -\frac{r_0^2}{2r} \cdot \frac{\partial B_{ac}}{\partial z}$$

$$B_{ac} = \frac{\mu r_0^2}{2} \frac{\partial^2 B_{ac}}{\partial z^2} \int_{r_0}^r \frac{dr}{r}$$

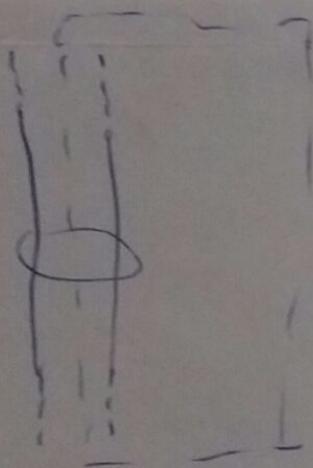
Since we approximated the flux we can take the upper limit to an order of λ

$$\lambda = \sqrt{\mu} r_0$$

$$B_{ac} = \frac{M r_0^2}{2} \frac{\partial^2 B_{ac}}{\partial z^2} \ln \sqrt{\frac{M}{2}}$$

$$\approx \frac{Mr_0^4}{4} \frac{\partial^2 B_{ac}}{\partial z^2} (\ln M) \Rightarrow$$

$$B_{ac} = A e^{-\frac{z}{r_0 \sqrt{\frac{M}{4} \ln(\mu)}}}$$



$$\oint \vec{H} \cdot d\vec{l} \Rightarrow 2 \int_0^\infty B_{ac} dz = \mu \mu_0 I$$

$$A = \frac{\mu \mu_0 I}{2 r_0 \sqrt{\frac{M}{4} \ln(\mu)}}$$

$$A = \frac{\mu \mu_0 I}{r_0 \sqrt{M \ln(\mu)}}$$

$$L = \frac{r_0 A}{I} = \frac{\mu_0 M r_0}{\sqrt{M \ln(\mu)}} = \mu_0 M r_0 \sqrt{\frac{M}{\ln(\mu)}}$$